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LINER EXPANDER

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Granted to Pan American Petroleum Corporation, Tulsa, Oklahoma, U.S.A.

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PRIORITY DATE

No. OF CLAIMS

LINER EXPANDER

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This invention relates to a constant force spring device, and more particularly, to a device for expanding a metallic liner wherein an expanding die is urged against the liner by a constant force spring device.

Heretofore, a method and apparatus have been developed for installing an expanded metallic liner in an oil well or other conduit. Typically, a corrugated steel liner is inserted in a conduit which is to be lined, the greatest peripheral dimension of the liner being slightly less than the inside diameter of the conduit. An expanding tool is passed through the liner placed in the conduit, and a first-stage expanding die causes a gross plastic deformation of the liner, which is expanded outwardly against the inside of the conduit. A second-stage die on the tool then provides an additional finer deformation of the liner to provide a smoother, more finished surface on the inside of the liner and to assure more complete contact between the conduit and the liner. In a typical design of this type expanding tool, the frictional drag of the first-stage die supplies the expanding force for the second-stage die, which expanding force is a direct function of the strength, or wall thickness, of the conduit in which the liner is being installed. For example, in lining oil well casing, heavy wall casing may cause a very high frictional force which results in excessive pressure being required to push the expander through the liner. The application of the great forces required may result in rupture of the casing or in breaking the installing tool. In instances where the internal diameter of the conduit is somewhat less than that anticipated, the resulting forces can cause the tool to become stuck in the casing, or otherwise cause damage to the casing and the tool. In other designs, such as where a cantilever spring arrangement is employed in connection with the secondstage die, various difficulties are encountered in obtaining a spring mechanism having the desired strength in combination with the other spring characteristics, and with the tool dragging against the inside wall of the conduit after being passed through the liner.

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Since tools of the type mentioned above often are employed in wells deep in the ground, it is highly preferable that a tool be used which under no circumstances will become stuck in the well or cause damage to the well. Any such trouble occurring in a well can result in considerable loss in time and great expense in making repairs.

An object of the present invention is a device for applying a constant force to an expanding die or other similar apparatus so that a preselected maximum force is exerted against a work piece. Another object is an improved expanding tool for installing metallic liners in a conduit, which expanding tool can apply no greater than a predetermined force to the liner being installed in the conduit. Still another object of the invention is an economical and easily fabricated constant force spring device. A further object is a rugged, easy-to-operate expanding tool employing such a spring device. These and other objects of the invention will become apparent by reference to the following description of the invention.

In accordance with the present invention there is provided a constant force spring device which comprises a body member, an elongated column element adjacent said body member, bearing plate members contacting the two ends of said column at least one of said bearing plate members being longitudinally movable in respect of the other and stop means on said body member to limit the deflection of said column element to prevent permanent deformation of said column element upon the application of a compressive load thereto. In one embodiment of the invention, the foregoing constant force spring device is employed in a tool for expanding a metallic liner inside a conduit, said constant force spring device being positioned on said tool to urge an expanding die member against the liner being installed in the conduit by a substantially constant force.

My invention will be better understood by reference to the following description and the accompanying drawings wherein:

Figures 1A, 1B and 1C, taken together, constitute a partial sectional view of a preferred embodiment of a liner expanding tool according to the present invention; and

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Figure 2 is a sectional view of the apparatus of Figure 1A taken at line 2-2; and

Figure 3 is a typical plot of applied Load versus Deflection for the constant force spring device of the invention.

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Referring to the drawings, Figure 1A is the bottom portion of a liner expanding tool for use in installing a metallic liner in a well, while Figure 1B illustrates the middle section of such a tool and Figure 1C represents the upper section of the tool. The expanding tool 11 is attached to standard well tubing 12 by coupling 13 and, typically, may be lowered from the surface through a well casing (not shown) to a point in the casing at which it is desired to install a metallic liner. Before inserting the tool into the well, an elongated vertically corrugated liner 14 fabricated from mild steel, or other suitable malleable material, is placed on the tool. The corrugated liner is secured in position by contact at its upper end with a cylindrical shoulder member 16 and, at its lower end by contact with a first-stage expanding die 17 in the form of a truncated circular cone which serves as a firststage expanding die in the manner hereinafter described. The expanding die is fixedly attached to a centrally located, elongated cylindrical hollow shaft 18 which forms a portion of the body of the tool. As shown, the expanding die 17 is held in place between a lower shoulder 19 and collar 21 threaded onto the shaft. A plurality of movable arms 22, preferably provided with outwardly enlarged portions 23 near the top, are disposed in the form of a cylinder around shaft 18. The enlarged portions of the arms 23 upon being moved outvardly contact the liner to perform the final step of expanding the corrugated liner into a substantially cylindrical shape. The arm members 22 are pivotally attached to the shaft so as to be movable outwardly from the shaft by a tapered expanding member 24 slidably positioned on the shaft to serve as a second-stage expander. The surface of the member 24, as shown, moves upwardly along the shaft to engage with the arms and move them outwardly. Advantageously, the inside surfaces of the arms 22 and the outside surface of expanding member 24 form mating sections, typically octagonal in shape. The expansion of the arm members is controlled by the position of the member 24 which moves upwardly

until it contacts shoulder 26 provided on the shaft. As member 24 moves in a downwardly direction arms 22 fold inwardly toward the shaft. The expanding arms 22 are held in place on the shaft by collar 27 and circular groove 28 provided on the shaft.

The expanding tool, comprising the first-stage die and the secondstage die is drawn through the liner to expand it in place in the casing. The
first-stage die provides a gross deformation of the liner so that it is
expanded outwardly against the wall of the casing. The second-stage die then
passes through the liner and performs the final expansion to smooth the inner
surface of the liner and to provide more even contact between the liner and
the wall of the casing and effect a fluid-tight seal.

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In operation, the liner setting tool is assembled at the surface, as described above, and a glass cloth saturated with a resinous material may be wrapped around the corrugated tube to form the liner. The assembly is lowered into the well at the location at which the liner is to be set. A liquid, such as oil, is then pumped under pressure down the well tubing and flows through the passageway 29 provided in polished rod 31, through ports 32 and into cylinder 33 connected to the upper end of the shoulder 16. Upon the application of fluid pressure to the cylinder, the piston 34 secured to polished rod 31 moves upwardly in cylinder 33. As shown, rod 36 connects polished rod 31 and shaft 18 upon which is mounted the first-stage expanding die 17. When the piston 34 moves upwardly through the cylinder 33 the expanding die 17 and the secondstage die 22 are drawn upwardly into the corrugated liner 14 and "iron out" the corrugations in the liner, so that the expanded liner may contact the inside wall of the casing in which it is being installed. Positioned on the shaft below the expanding member 24 is a constant force spring member 37 which is employed to urge the expanding member against the expanding arms 22 with a substantially constant force. The force exerted against the arm members being substantially constant, the force transmitted through the arm members to the liner and to the casing will be substantially constant so that either sticking of the tool in the casing or rupture of the casing is precluded. Of course, the force provided by the spring member is preselected so that the frictional

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forces between the tool and the liner and the pressure exerted against the casing are maintained at predetermined safe levels. The constant force spring member assures that the contact pressure between the liner forming portion 23 of the arms 22 is great enough to provide the desired deformation of the casing, while preventing damage to the casing or to the tool.

The constant force spring member 37 is slidably mounted on the shaft 18 and held between the expanding element 24 and a cylindrical lower shoulder member 38 forming a portion of a differential sorew element 39 which transmits the loading on spring member 37 to shaft member 18. The differential screw element comprises shaft member 18 on the outside of which are cut male threads 18a, the lover shoulder member 38 provided with female threads 38a and thimble member 41 provided with threads 41a and 41b on the outside and the inside, respectively, to engage with threads on the shaft and the shoulder. The two sets of threads are coarse, such as square, modified square, or Acme threads, to withstand very high loads and differ in pitch so that shoulder 38 is moved upwardly on the shaft 18 when the shaft is revolved relative to thimble 41. The shoulder 38 is secured to the shaft 18 by splines 45 so that it can slide longitudinally, but it is not free to rotate on the shaft. Fixedly attached to the lower end of the thimble is a friction member, such as bow springs 42, a hydraulically actuated friction pad, or other such device for frictionally engaging with the inside wall of the conduit to secure the thimble against rotation with respect to the shaft. Preferably, the direction of the shoulder member threads 38a is the same as that of the shaft threads 18a, e.g. righthand threads, and the pitch, or lead, of threads 18a is slightly greater than that of threads 38s, with the pitch ratio being close to unity. In this manner, clock-wise revolution of the shaft relative to the thimble causes shoulder member 38 to advance upward slightly and a compression load is exerted upwardly on spring element 37 to cause buckling. For example, one satisfactory differential screw was made up using five and one-half threads/inch square threads on a shaft approximately 1.7-inch outside diameter and five and threequarters threads/inch square threads on a shoulder approximately 2.5-inches inside diameter.

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Constant force spring element 37 comprises column element 43, advantageously consisting of a plurality of elongated columns disposed around shaft 18. Upper bearing plate member 44 is in contact with the upper ends of the columns and is slidably positioned on shaft 18 to transmit the force of the spring longitudinally against the bottom end of expander member 24. Lower bearing plate member 46 contacts the lower ends of the columns and is moved upwardly along the shaft by longitudinal movement of lower shoulder 38 as a result of revolving differential screw element 39. Grooves 47 are provided in each of the bearing plates, to form an upper race and a lower race, into which the ends of the columns are inserted. These grooves may be shaped to conform with the shape of the column ends if desired. A cover 48 may be employed to exclude foreign matter from the spring mechanism and to protect the spring.

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A means for limiting the deflection of the columns is required. Although the column element functions in a buckled condition, application of excessive compressive load thereto would cause total failure or rupture of the columns. Therefore, a pair of stops 49 and 49s are provided for this purpose. As shown, the stops are rigidly connected to the bearing plates, and, in effect comprise upper and lower limiting sleeves positioned on the shaft to slide longitudinally thereon. The ends of the stops may move toward, or away from, each other as the load on the spring member varies. Lower sleeve 49a is prevented from moving down by lower shoulder 38 connected to the shaft 18. However, the spacing between the ends is such as to limit the longitudinal travel of the bearing plate members as they move together to prevent permanent deformation of the column element 43. Various alternative means for preventing damage to the column element may also be employed. For example, pins or rings mounted on the shaft may serve as stops, or the cover 48 provided with suitable connections may be employed for this purpose to limit longitudinal and/or lateral deflection of columns.

The columns of the column element 43 may be arranged around the shaft 18, which as shown here forms a portion of the body of the spring device, with ends of the columns fitted in the races 47. The columns may be

fitted closely together as shown, or may be spaced around the race, with separators used between them to maintain the desired spacing. The number of columns employed will depend upon column characteristics and the materials of construction. For example, the slenderness ratio of the column may be varied widely, and the column ends may be round, flat, fixed or hinged. The preferred construction is a thin, slender column with rounded ends, free to move within the races shaped to the curvature of the column ends. Materials which may be satisfactorily employed for the columns are carbon and low alloy steels, chromium and nickel-chromium stainless steels, various copper base alloys, such as phosphor bronze, beryllium copper, the high nickel alloys and other similar materials providing satisfactory mechanical properties. Typically, the individual columns are of long rectangular cross-section, with the width being greater than the thickness, and arranged so that the wider face of the columns is normal to the diameter of the shaft. Thus, with sufficient compression loading, the columns buckle, and bend about the axis having the least moment of inertia, e.g., outwardly away from the shaft ld.

For example, a group of columns 0.167-inch thick by 0.438-inch wide by 10.626-inches long, with the ends rounded, were fabricated from A.I.S.I 4340 steel, quenched and drawn at 575°F. Each column was found to require a 20 critical compression loading of 450 pounds in order to buckle the column. After buckling, the columns were found to have a very flat spring characteristic, as shown in Figure 3, wherein $P_{\rm c}$ is the critical buckling load and point C represents the load and deflection at which the stress in the extreme fibers of the column exceed the yield point of the material. Theoretically, the shape of this spring characteristic curve is described by curve OA'ABC. Actually, this curve is described by OABC due to friction in the system. Points A end B represent typical working limits, which, of course, may be varied according to the application for which the spring is designed. For example, where a large number of flexing cycles are not anticipated, a working stress just below the 30 yield point may be used, while with a great number of flexures, the working stress may be held to less than the endurance limit of the material of construction. In the above-mentioned tests, the lateral deflection was limited to

approximately one inch, at which the longitudinal deflection was approximately: 0.225 inches. From zero deflection to the maximum deflection, the 450-pound loading was found to be substantially constant.

In another test a spring device was built, as shown, employing 20 columns, each having a critical buckling load of 1250 pounds. The lateral deflection was limited between 0 and about 1.00 inches by appropriately positioning the stops. Upon compressional loading, the spring element buckled at substantially 25,000 pounds and from a longitudinal deflection of 0.04 inches (buckling) to about 0.15 inches the load remained substantially at 25,000 pounds.

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Of course, in designing a spring element as above it is advantageous to obtain the greatest possible value of longitudinal deflection for specified values of lateral deflection and critical buckling load, while maintaining the stress level in the columns at a safe level. The preferred columns, therefore, are laminated, as shown in Figures 1B and 2, with multiple flat members making up each column.

In the operation of the above expanding tool for setting a liner in well casing, the made-up tool is lowered into the well as mentioned above, with the arms 22 in the retracted position. When the tool is at the desired level, the well tubing is revolved. The friction member 42 engages with the wall of the casing and prevents thimble 41 from revolving. With several revolutions of the tubing, lower shoulder 38 is moved upwardly by differential screw 39 to buckle spring element 37 which has a predetermined critical buckling load. This load is transmitted upwardly against the lower end of expander 24, and its tapered surface is engaged with the tapered surface on the inside of the arms 22 to urge the arms outwardly with a substantially constant force proportional to the critical buckling load of the spring element. Subsequently, the expanding tool is passed through the liner to expand it in the casing in the manner described hereinbefore.

The foregoing description of a preferred embodiment of my invention has been given for the purpose of exemplification. It will be understood that various modifications in the details of construction will become apparent to

the artisan from the description, and, as such, these fall within the spirit and scope of my invention.

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I CLAIM:

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- 1 1. A device for expanding a metallic liner inside a conduit which device comprises a shaft element, an expanding die member attached to said 2 shaft element, said die member comprising a movable liner-forming member 3 positioned on said shaft and being radially movable in respect thereof to contact said liner, an expander member slidably positioned on said shaft 6 between said shaft and said die member to move said liner-forming member from said shaft, and a constant force spring member positioned on said shaft 7 8 to contact said expander member and to maintain said expander member against said liner-forming member, whereby said liner-forming member is urged against 10 said liner by a substantially constant force.
- 1 2. In a device for installing an expanded metallic liner in a conduit wherein an expanding die is moved through a liner positioned in said conduit to expand said liner: a cylindrical shaft element, an expanding die member attached to said shaft, said die member comprising a plurality of arm members disposed around said shaft and being pivotable outwardly therefrom to contact said liner, a cone member slidably positioned on said shaft between said shaft and said arm members to urge said arm members outwardly from said shaft, and a constant force spring member positioned on said shaft to contact said cone member and to maintain said cone member in contact with said arm members, whereby said arm members are urged outwardly by a substantially constant force.
 - 3. The device of Claim 2 wherein said constant force spring member comprises a plurality of columns disposed around said shaft, a first bearing plate member and a second bearing plate member, each of said bearing plate members contacting opposite ends of said columns, at least one of said bearing plate members being movably positioned on said shaft and being in contact with said come member, stop means connected to said shaft to limit the axial travel of said movable bearing plate member along said shaft, and compression means for maintaining a lateral deflection in said columns.

- 1 4. The device of Claim 3 wherein said compression means comprises
 2 a differential screw connecting said spring member and said shaft.
- 5. The device of Claim 3 wherein said stop means comprises a sleeve-like element connected to said movable bearing plate member and slidably positioned on said shaft and a member connected to said shaft to limit the travel of said sleeve-like element.
- 6. The device of Claim 3 wherein said columns have a rectangular cross-section, the width being greater than the thickness, and having the wider face normal to the diameter of said shaft.
 - 7. A device for installing an expanded metallic liner in a conduit which comprises a cylindrical shaft element; an expanding die member mounted on said shaft, said die member comprising a plurality of arm members disposed circumferentially around the outside of said shaft and being pivotable outwardly therefrom to contact the liner; a conical expanding member slidably positioned on said shaft between said shaft and said arm members to urge said arm members outwardly from said shaft; a plurality of slender columns, each having a long rectangular cross-section and disposed circumferentially about said shaft; an upper bearing plate member and a lower bearing plate member, each slidably positioned on said shaft and contacting opposite ends of said columns; limiting sleeves attached to each of said bearing plate members and slidably positioned on said shaft; a shoulder member on said shaft; a differential screw element connecting said shoulder and said shaft to apply a buckling load to said columns; said shoulder being engageable with the limiting sleeve connected to said lower bearing plate member, whereby the axial travel of said bearing plate members is limited; said column members transmitting their buckling load to said arm members to urge said arm members outwardly with a substantially constant force.

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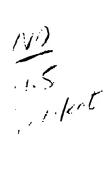
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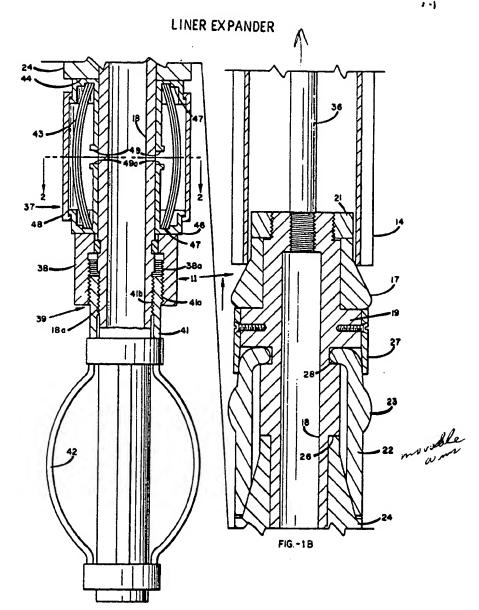
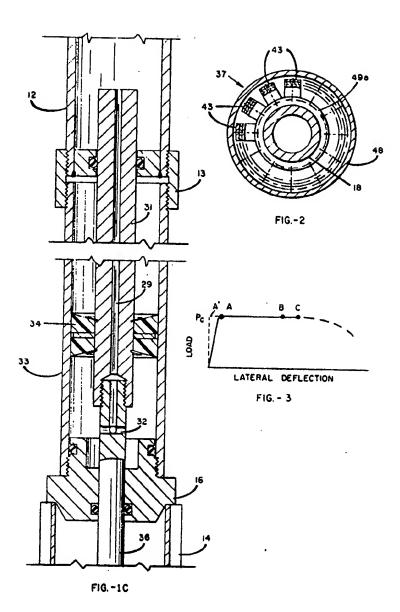


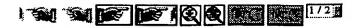
FIG.-1A



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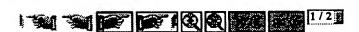
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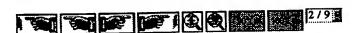




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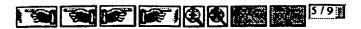


until it contacts shoulder 25 provided on the chaft. As number 24 wower in a documently direction area 22 feld invertily towers the shaft. The expending area 22 are held in place on the shaft by collect 27 and circular groups 20 recorded on the shaft.

The expending tent, comprising the first-stage die and the seatchstage die to drewn through the liner to expend it in place in the caning. The first-stage die provides a gross differention of the liner so that it is expended outworthy against the wall of the seeing. The second-stage die them passes through the liner and performs the first agreement to smooth the liner surface of the liner and to provide more even contact between the liner and the wall of the caning and effect a finid-tight soal.

In operation, the liner setting tool is assembled at the surface, so described shows, and a glass cloth saturated with a revisions material may be unapped around the corrugated take to form the liner. The assembly is lovered into the well as the incention at which the liner to to be set. A liquid, such so oil, is then pusped under presume down the well inhing and flows through the passegmany 29 provided to polished rot 31, through purts 52 and into equiader 35 consected to the upper end of the aboulder 16. Upon the application of fluid procesure to the cylinder, the pistes 34 secored to polished red 31 moves specially in ordinates 55. As shown, not 36 corescuts political rod 31 and shaft 15 spon shigh is nowbed the first-stage expending die 17. Then the piston % eartly through the sylindar 33 the expending die 17 und the secondstage die 22 are draus upwardly into the corrugated liner 18 and "iron out" the corregations in the liner, so that the expected liner may contect the incide well of the casing in which it is being installed. Positioned to the shaft below the expending member th is a communit terms spring number 37 which is employed to trips the expanding number against the explosing some 22 with a substantially sometant force. The force exacted against the are needers being substantially sometant, the force transmitted through the arm members to the lists and to the during will be substantially-accordant on that either sticking of the tool in the casing or rupture of the casing to precluded. Or course, the chron provided by the spring menter is preselected so that the frictional





forces between the tool and the liner and the presence exerted ageinst the eming are extintained at presentational safe levels. The constant force spring maker exerces that the contact presents between the liner founday portion 25 of the sons 22 is great ecough to provide the derived deformation of the staing, while preventing designs to the easing or to the tool.

The especiant force spring seasor 77 is alignity nounted on the shall like and hald between the expending alongst 20 and a cylindrical lower checker number 10 forming a portion of a differential screw alongst 29 which transmits the looking on spring number 77 to chart member 18. The differential screw alongst comprises shall number 18 on the certific of uniah are sub-mile transfe. 18st, the lower shaller number 18 provided with funcio threads 50s and thinkle number b) provided with threads ble and h)b on the certific set. the leading respectively, to supage with threads on the shall only the shoulder. The two sets of threads are meares, such as square, modified equare, or force threads, to vitarized very high loads and differ in pitch so that shoulder 30 is seven appearing on the shaft 18 when the shaft is revolved relative to thinkle \$1. The obsolutor 30 is severed to the shaft is revolved relative to thinkle \$1. The obsolutor 30 is severed to the shaft 18 by splines 55 so that it can alide longitudinally, but it is not tree to rotate on the shaft. Finally areached to the lower and of the thinkle is a friction number, such as but springs \$2, a hydranilously equated friction pass, or other such device for frictionally empaging with the issues will of the anniest to occurs the thinkle against toolation with respect to the shaft. Preferably, the direction of the shoulder number 18 to shoulder when the shoulder when the pitch, or long, of arreads 10s is a slightly greater than the of threads 30s, with the pitch, or threads 10s is a slightly on a compress 10 to alwance appears alightly and a compression loud in americal squarely on apring alament 37 to assect bacting. For example, one vertificatory introdes un a chart approximately 1.7-inch outside dissector and five and invasion quarters threads/inch aquare threads on a shoulder approximately 2.5-inches inside dissector.



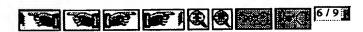


Donatest force spring element 37 comprises union element 15, aivactageonally constinting of a plurality of alongsted columns disposed around shaft
18. Upper bearing plate number th is in contant with the appearance of the
solume and is elitably positioned on shaft 18 to transact the force of the
spring longitudinally against the bottom and of expender senters th. Lower
bearing plate number 16 contacts the lover sents of the columns and is noved
specially along the sanft by lengthedizal movement of locar sacraider 38 on a
result of revolving differential movement 39. Greenes 17 see provided
in sents of two bearing plates, to form an upper sans and a lover mess, into
which the easts of the columns are inserted. These greenes may be shaped to
senters with the shape of the column mote if sactivel. A cover 18 may be
suplosed to account forwign uniter from the spring mechanism such to protect

A seems for limiting the defination of the columns is required. Although the column element functions in a buckled condition, application of . proceeds nonpressive load thereto would came total failure or reptare of the solume. Therefore, a pair of stope by see by one by one provided for this purpose. As shown, the stope ere rigidly connected to the bearing plates, and, in effort comprise upper and lower limiting slacres positioned on the shaft to alide longitudinally thereon. The undo of the stope may move toward, or may from, each other so the look in the spring number vertes. Lover slaves bya is presented from moving does by igner shoulder 55 someouted to the short 18. z, the speciag between the sade is much as to limit the longitudinal of the bearing plate members on they more together to prevent permu deformation of the column alement \$3. Maximum alternative means for preventing damage to the column element may also be employed. For example, pink or rings someted on the chaft may serve as stops, or the cover 48 provided with suitable connections may be suplayed for this purpose to limit longitudical and/or lateral saffection of columns.

The columns of the column classes 43 may be arranged eround the shart 15, which as shown here turns a portion of the body of the spring Series, with made of the columns fitthed in the reces 57. The solumns may be

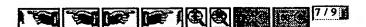
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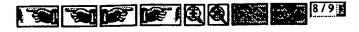




ritted closely together as shors, or may be spared around the race, with separators used between these to maintain the desired spacing. The resolut of construction. For example, the elementers ratio of the column may be varied without, set the column solutes may be record, flat, fines or hisped. The preserved construction is a thin, element column with tousiest ands, from to now within the races shaped to the coresiste of the column cole. Internals which may be notified visited to the coresiste of the column cole. Internals which may be notified voterly suplayed for the column are covien and low allow steels, chronium and alcohal-chronium stainless whom, serious support how allians, such as passagher bronze, beryllium support, the high stabel allows and other similar externals providing attificatory mechanismi properties. Typically, the individual solutes are or long rectangular cross-cention, with the stath being greater then the lakehouse, and accomped so that the wider face of the unisme is sormal to the simular of the abort. Thus, with surfacient consensation lossing, the column buckle, and tund shout the arise hering the loars soment of inartia, e.g., outrarily may from the shaft 18.

For example, a group of columns 0.161-inch thick by 0.435-inch wife by 10.626-inches long, with the ends rouseled, were fabricated from 1.1.8-I 4360 steel, quesabed set draws at 575°F. Duch column was found to require a critisel suspension loading or M50 pounds in order to bankle the address. . After buckling, the columns were found to have a very flat spring characteristhe, as shows in Figure 3, therein Pa is the critical beauting look and point mie the load and deflection at which the stress is the extreme fibers delines exceed the yield point of the untertal. Theoretically, the chape of this spring characteristic curve is decurited by eners CA'ABC. Actually, Unis curve is described by OMSC due to friction in the system. Potesta A and S represent typical strking limits, which, of course, may be varied according to the application for which the spring is designed. For example, where a large ber of flexing speles are not sociolysted, a working stress just below the 30 yield point may be weed, while with a great number of flaures, the working stress may be held to less than the enfurence limit of the enterial of score tion. In the above-mentioned tests, the lateral deriection was limited to





Approximately one truck, at which the longitudinal defloration was approximately 0.225 inches. From more deflection to the assistant deflection, the \$50-pound loading was fromt to be substantially constant.

In smother test a spring durine was built, as down, employing 80 columns, each having a critical buckling load of 1250 younds. The internal deficience was limited between 0 and about 1.00 inches by emprogrately positioning the steps. Once compressional loading, the spring whemset buckled at admirately 25,000 possets and from a lengthelism! defication of 0.0k inshes (making) to stout 0.15 inches the lend remained substantially at 25,000 possets.

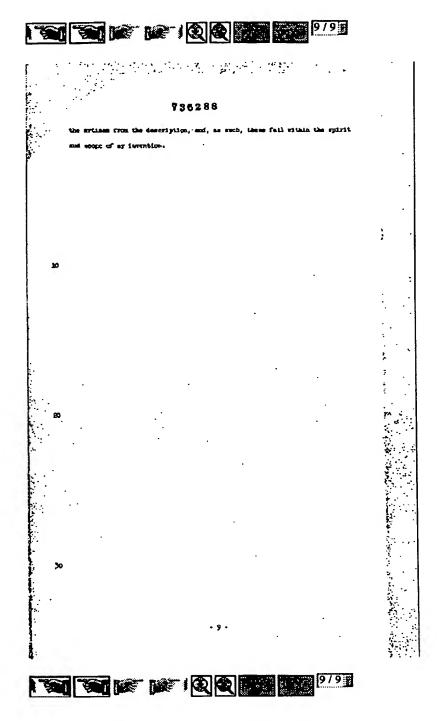
Of course, in dorigating a spring vicenation above it is advantageous to driven the greatest possible value of longitudinal Sectionism for specified values of laboral deflection and article bushing load, while unintening the stress level is the columns at a safe level. The preferred columns, therefore, are laminated, as shown in Figures 13 and 2, with unitiple flat mediate units we seek column.

In the operation of the shows expecting tool for setting a liner in well encised, the mede-up tool is lowered into the sell as sectional shows, with the area 22 in the retreated position. Then the tool is at the desired level, the well tolding is revolved. The friction number he capages with the wall of the enting and prevents thinkle hi from revolving. With several revolutions of the tables, lower shoulder 15 is nowed assembly by differential server 39 to buddle spring almost 37 which has a predefending writinal buddling love. This last is transmitted assembly against the lower and of expender 16, and the tapered surface is engaged with the tapered surface on the incides of the sum at to args the loves enterethy with a substantially constant force proportional to the critical bucking load of the spring almost. Extengently, the expending tool is passed through the lines to expend it in the caping is the means described hereishefore.

the foregring description of a preferred embalished of an investigahas been given for the purpose of examplification. It will be understood that vertoes madifications in the detects of exceinanties will become apparent to

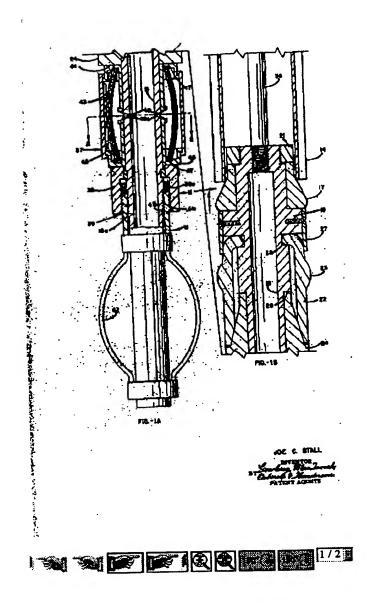
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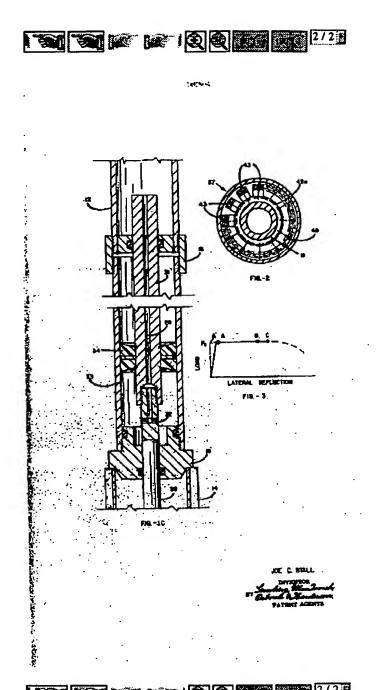






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